

Lecture 2 : Castigliano's

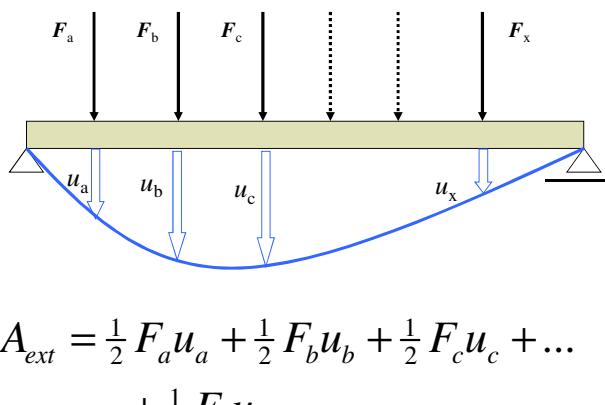
Energy Theorems

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v2021-1

http://icozct.tudelft.nl/TUD_CT/

Castigliano



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Differentiate the Work to a specific force, e.g. F_x :

$$\frac{\partial A_{ext}}{\partial F_x} = \frac{1}{2} F_a \frac{\partial u_a}{\partial F_x} + \frac{1}{2} F_b \frac{\partial u_b}{\partial F_x} + \frac{1}{2} F_c \frac{\partial u_c}{\partial F_x} + \dots$$

$$+ \frac{1}{2} u_x + \frac{1}{2} F_x \frac{\partial u_x}{\partial F_x}$$

Use Maxwell's notation :

$$u_a = c_{aa} F_a + c_{ab} F_b + c_{ac} F_c + \dots + c_{ax} F_x$$

$$u_b = c_{ba} F_a + c_{bb} F_b + c_{bc} F_c + \dots + c_{bx} F_x$$

$$u_c = c_{ca} F_a + c_{cb} F_b + c_{cc} F_c + \dots + c_{cx} F_x$$

$$u_x = c_{xa} F_a + c_{xb} F_b + c_{xc} F_c + \dots + c_{xx} F_x$$

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Elaborate for all ...

$$\frac{\partial u_a}{\partial F_x} = \frac{\partial(c_{aa} F_a + c_{ab} F_b + c_{ac} F_c + \dots + c_{ax} F_x)}{\partial F_x} = c_{ax}$$

$$\frac{\partial u_b}{\partial F_x} = \frac{\partial(c_{ba} F_a + c_{bb} F_b + c_{bc} F_c + \dots + c_{bx} F_x)}{\partial F_x} = c_{bx}$$

$$\frac{\partial u_c}{\partial F_x} = \frac{\partial(c_{ca} F_a + c_{cb} F_b + c_{cc} F_c + \dots + c_{cx} F_x)}{\partial F_x} = c_{cx}$$

$$\frac{\partial u_x}{\partial F_x} = \frac{\partial(c_{xa} F_a + c_{xb} F_b + c_{xc} F_c + \dots + c_{xx} F_x)}{\partial F_x} = c_{xx}$$

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Result:

$$\frac{\partial A_{ext}}{\partial F_x} = \frac{1}{2} F_a c_{ax} + \frac{1}{2} F_b c_{bx} + \frac{1}{2} F_c c_{cx} + \dots + \frac{1}{2} F_x c_{xx} + \frac{1}{2} u_x$$

Maxwell :

$$c_{ax} = c_{xa}$$

$$c_{bx} = c_{xb}$$

$$c_{cx} = c_{xc}$$

Castigliano's 2nd theorem

$$\boxed{\frac{\partial A_{ext}}{\partial F_x} = \frac{1}{2} c_{xa} F_a + \frac{1}{2} c_{xb} F_b + \frac{1}{2} c_{xc} F_c + \dots + \frac{1}{2} c_{xx} F_x + \frac{1}{2} u_x}$$

$$\boxed{\frac{\partial A_{ext}}{\partial F_x} = u_x}$$

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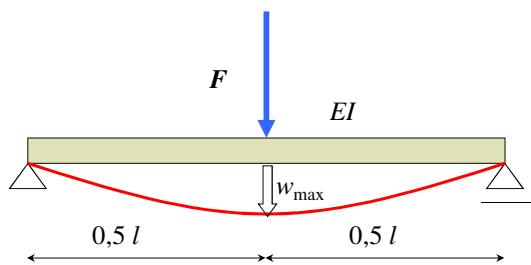
Castigliano

- Work done by external loads A_{ext} is stored in the strain energy E_c (complementary)
- Differentiate the strain energy to a force at location x to find the displacement u at x

$$\boxed{\frac{\partial E_c}{\partial F_x} = u_x}$$

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Example



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Strain Energy in terms of the load

$$M(x) = \frac{1}{2} Fx \quad 0 \leq x \leq \frac{1}{2}l$$

$$E_c = \int_0^l \frac{M(x)^2}{2EI} dx = 2 \int_0^{\frac{1}{2}l} \frac{\frac{1}{4}F^2x^2}{2EI} dx = \frac{F^2l^3}{96EI}$$

$$w = \frac{dE_c}{dF} = \frac{2Fl^3}{96EI} = \frac{Fl^3}{48EI}$$

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Steps of the solution strategy

- Castigliano : differentiate E_C to a force.
- E_C is integral of the square of the moment distribution
- so
.... differentiate after integration ...
IS THIS SMART TO DO ??

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Smart help

$$w = \int_0^l \frac{m(x) \times M(x)}{EI} dx$$

$$w = \int_0^l \frac{2M(x)}{2EI} \times \frac{dM(x)}{dF} dx = \int_0^l \frac{M(x)}{EI} \times \boxed{\frac{dM(x)}{dF}} dx$$

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Castigiano

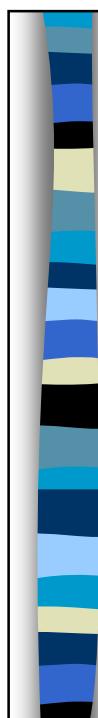
- Second theorem

$$\frac{\partial E_c}{\partial F_x} = u_x$$

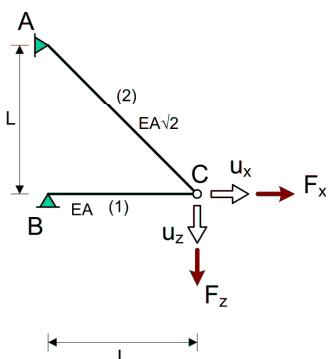
- First theorem

$$\frac{\partial E_v}{\partial u_x} = F_x$$

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Application



$\frac{\partial E_v}{\partial u_x} = F_x$
(energy expressed in u_x and u_z)

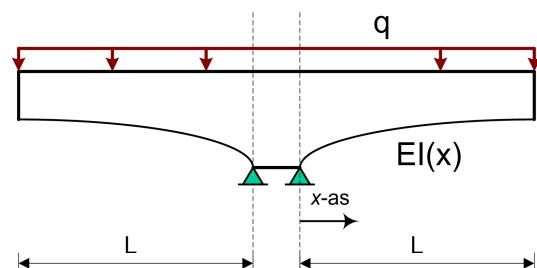
$\frac{\partial E_c}{\partial F_x} = u_x$
(energy expressed in F_x and F_z)

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Example

deformation with Castigliano:

- Find the displacement at the free end
- Find the rotation at the free end



Given :

$$EI(x) = EI_o \left(1 - \frac{x}{l}\right); \quad EI_o = 150 \times 10^6 \text{ kNm}^2; \quad l = 40 \text{ m}; \quad q = 35 \text{ kN/m}$$

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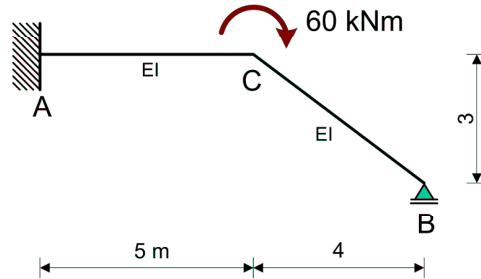
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Example

Force distribution with Castigliano:

- Find the support reaction at B using Castigliano
- Draw the moment distribution



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Application : shear stiffness

Beam:

- Axial loading
- Bending
- Shear**
- Torsion

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Asumme LE, find k

discrete model

$$E_v = E_c = \frac{1}{2}V \times dw = \frac{1}{2}V \times \gamma_1 \times dx$$

with: $V = k \times \gamma_1$

continuous model

Shear stress distribution not constant over depth
If LE then shear strain γ not constant!

$$\tau = \tau_{\max} \left(1 - \left(\frac{2z}{h} \right)^2 \right)$$

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Equal amount of stored energy



discrete :

$$E_c = \frac{1}{2} V \times dw = \frac{1}{2} V \times \gamma_1 \times dx$$

continuous :

$$E_c = \int_{z=-h/2}^{z=h/2} \frac{\tau(z)^2}{2G} b dx dz$$

with : $\tau(z) = \frac{V \times S_z^{(a)}}{b \times I_{zz}} = \frac{6V}{bh^3} \left(\frac{h^2}{4} - z^2 \right)$

$$\int_{z=-h/2}^{z=h/2} \frac{\tau(z)^2}{2G} b dx dz = \frac{1}{2} V \gamma_1 dx$$

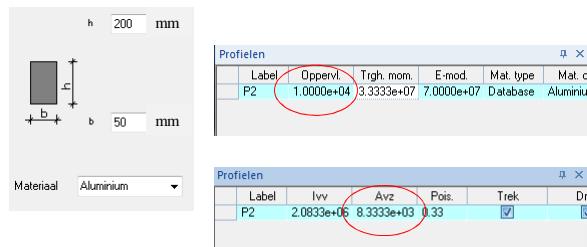
$$\frac{b}{G} \int_{z=-h/2}^{z=h/2} \tau(z)^2 dz = V \gamma_1$$

$$\frac{6V^2}{5Gb^h} = V \gamma_1 \Rightarrow \frac{V}{\gamma_1} = \frac{5}{6} Gb h$$

k = $\frac{5}{6} GA$ with: $G = \frac{E}{2(1+\nu)}$

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Analysis Software



Material: Aluminum

$A = b \times h = 200 \times 50 = 10000 \text{ mm}^2$

$A_{shear} = \frac{5}{6} \times 10000 = 8333,33 \text{ mm}^2$

$G = \frac{E}{2(1+\nu)}$ so: $GA_{shear} = \frac{GA}{\eta}$ with $\eta = \frac{6}{5}$

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Beam model with shear deformation

- Euler-Bernoulli – no shear deformation (one ODE)
- Timoshenko beam theory – bending and shear (two coupled ODE's)

CIE4190 Analysis of Slender Structures

$$EI \frac{d^4 w}{dx^4} = q(x)$$

$$EI \frac{d^2 \varphi}{dx^2} - GA_{shear} \left(\frac{dw}{dx} + \varphi \right) = 0 \quad (1)$$

$$GA_{shear} \left(\frac{d^2 w}{dx^2} + \frac{d\varphi}{dx} \right) = -q \quad (2)$$

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